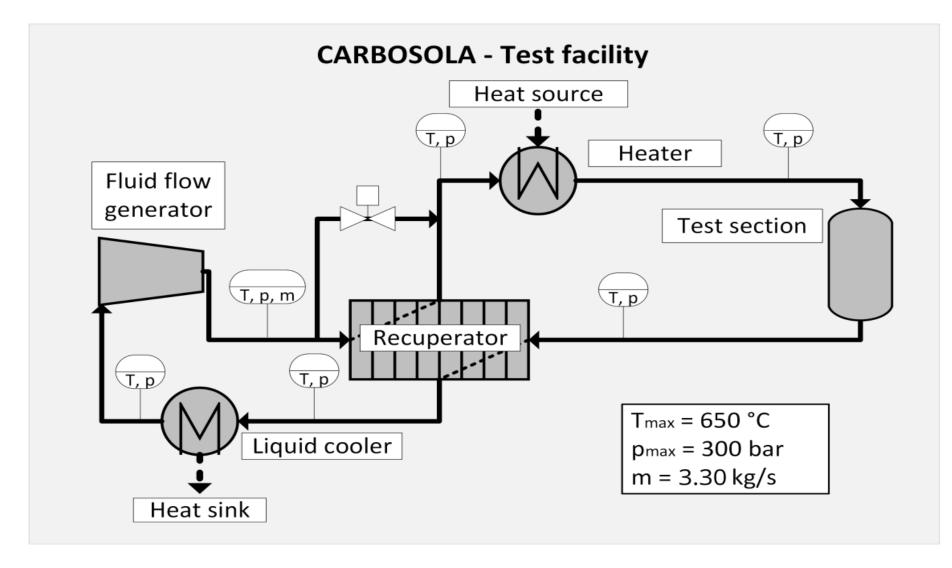


# Optimization and preliminary design of a hightemperature, low pressure-ratio sCO<sub>2</sub>-compressor for a wide operating range



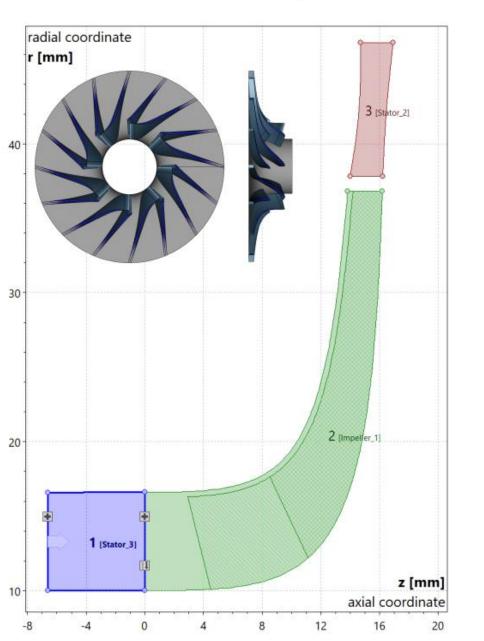
S. Rath, U. Gampe (Institute of Power Engineering, TU Dresden, Germany)
U.Hampel, S. Unger (Institute of Fluid Dynamics, Helmholtz-Zentrum Dresden-Rossendorf, Germany)

#### Motivation



- Experimental facility set up within the CARBOSOLA project (supercritical <u>carbon</u> dioxide as alternative working fluid for <u>bo</u>ttoming cycle and <u>solar</u> thermal application)
- First rig configuration without expansion device
   → pure fluid circulation at low pressure difference
- Design of a centrifugal compressor to provide fluid circulation over a wide operating range

# Baseline impeller design



| Mass flow                         | ṁ                    | 3.3      | kg/s   |
|-----------------------------------|----------------------|----------|--------|
| Total inlet temperature           | $T_{0,\mathrm{tot}}$ | (31) 200 | ° C    |
| Total inlet pressure              | $p_{0,tot}$          | 290      | bar(a) |
| Pressure ratio                    | $\Pi_{tot}$          | 1.035    | -      |
| Estimated tot. to tot. Efficiency | $\eta_{tt}$          | 0.85     | -      |
| Speed                             | $n_{RPM}$            | 18000    | rpm    |
| Work coefficient                  | $\psi$               | 1.18     | -      |
| Flow coefficient                  | $\varphi$            | 0.04     | -      |
|                                   |                      |          |        |
| <b>Hub diameter</b>               | $d_H$                | 20.0     | mm     |
| Suction diameter                  | $d_{\mathcal{S}}$    | 33.0     | mm     |
| Impeller diameter                 | $d_2$                | 72.0     | mm     |
| Outlet width                      | $b_2$                | 2.00     | mm     |
| Tip clearance                     | $x_{tip}$            | 0.35     | mm     |

- First impeller design based on the rig boundary conditions
- Parametrized geometry model using the design software
   CFturbo providing a direct export to CFD

# **Optimization criteria**

- Geometry optimization by varying 20 design parameters using a multi-objective genetic algorithm
- Numerical evaluation of each design in terms of a 3D, single blade passage CFD-model
- Operating range of each design estimated at the design point by the equivalent diffusion factor from 1D impeller theory:

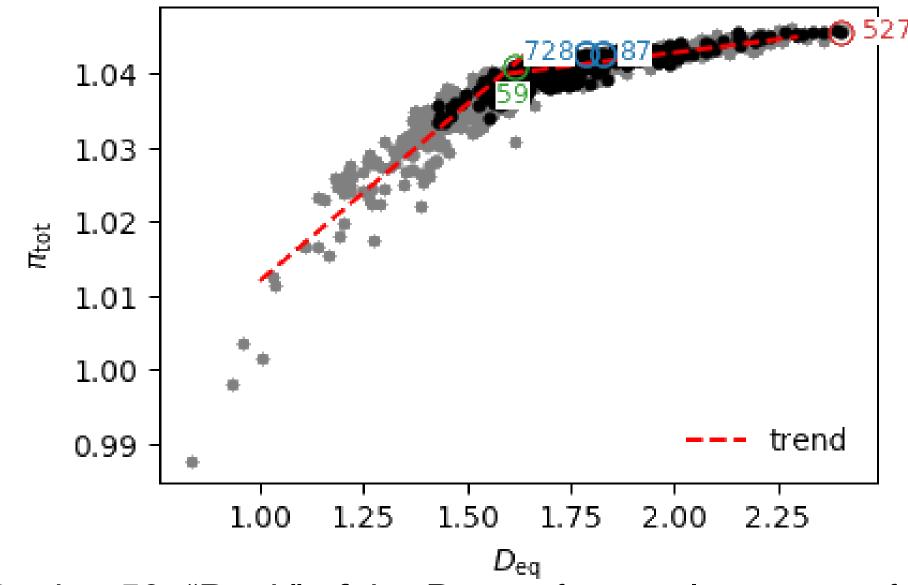
$$D_{\text{eq}} = \frac{w_{max}}{w_2} = \frac{1}{2 \cdot w_2} \cdot \left( w_1 + w_2 + \frac{2\pi \cdot d_2 \cdot u_2 \cdot I_B}{z_{\text{eq}} \cdot L_B} \right)$$

Full optimization target:

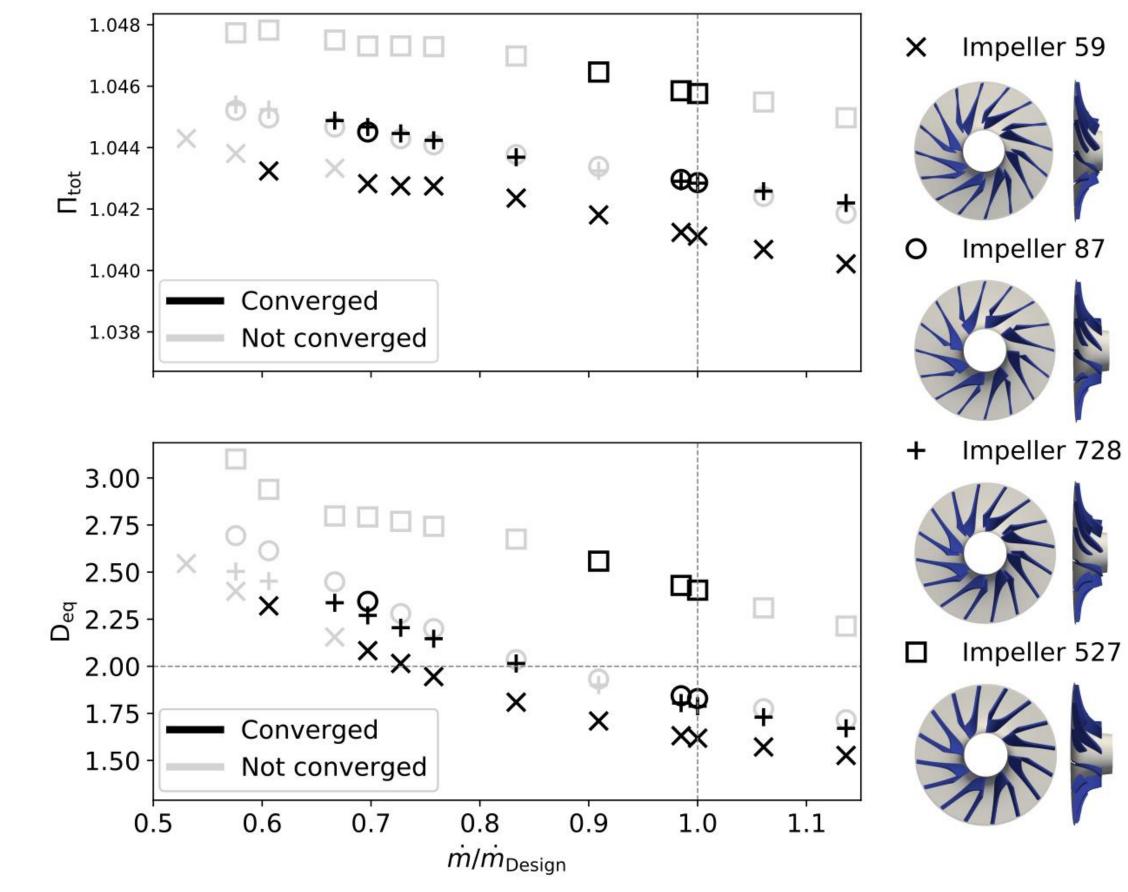
$$\min(D_{eq}) \wedge \min(w_2) | \pi_{tot} \ge 1.036$$

### **Optimization results**

- Evaluation of 1067 designs in total
- Selection of 4 designs with various  $D_{\rm eq}$  to verify the optimization target

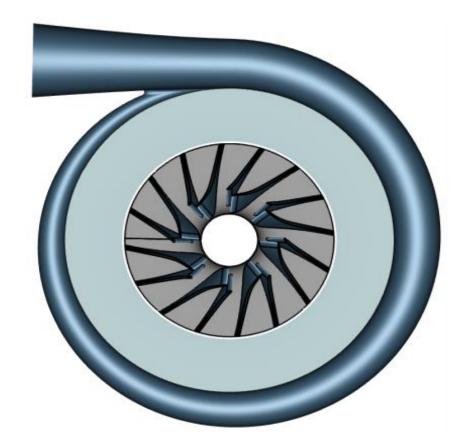


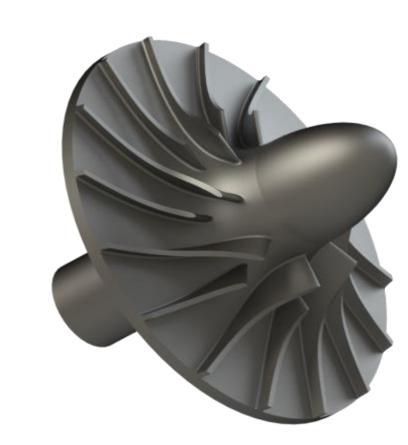
- Design 59: "Peak" of the Pareto front at lowest  $D_{\rm eq}$  from which only small changes in  $\pi_{tot}$  occur for higher  $D_{\rm eq}$
- Designs 728, 87: Compromise between higher  $\pi_{tot}$  and low  $D_{eq}$
- Design 527: Highest  $D_{eq}$



- Comparison of performance lines validates suitability of  $D_{\rm eq}$  to be used as an <u>indicator</u> for a wide operating range
- Differences for impeller 728 and 87 shows that  $D_{\rm eq}$  is an indicator but not a guarantee for a wide and stable range
- Impeller design 728 shows the best compromise of a wide operating range and high values for  $\pi_{tot}$

### Optimized design





Based on the selected impeller a solid model and a stage design were created for further evaluation

This work has been carried out within the project CARBOSOLA funded by the German Federal Ministry for Economic Affairs and Energy, grant reference: 03EE5001B.

